# Magetoresistance of RuO<sub>2</sub>-based resistance thermometers below 0.3 K

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#### Abstract

We have determined the magnetoresistance of  $RuO_2$ -based resistors (Scientific Instruments RO-600) between 0.05 K and 0.3 K in magnetic fields up to 8 T. The magnetoresistance is negative around 0.5 T and then becomes positive at larger fields. The magnitude of the negative magnetoresistance increases rapidly as the temperature is lowered, while that of the positive magnetoresistance has smaller temperature dependence. We have also examined the temperature dependence of the resistance below 50 mK in zero magnetic field. It is described in the context of variable-range-hopping conduction down to 15 mK. Hence, the resistors can be used as thermometers down to at least 15 mK.

*Key words:* thermometry at very low temperatures; thick-film chip resistors; magnetoresistance; ruthenium oxide resistance thermometers

# 1 Introduction

As promising low-temperature thermometers, RuO<sub>2</sub>-based thick-film chip resistors have been introduced (see for example Ref. 1). The advantages of such resistors are reproducibility and reasonably small magnetoresistance. In order to implement the accuracy of the thermometry in magnetic fields, a lot of work has been devoted to the magnetoresistance measurements of RuO<sub>2</sub>-based resistors [2–11]. Unfortunately, the magnetoresistance seems to be dependent on the detail of the manufacturing process. In the case of commercial resisters,

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results vary even in the sign of the magnetoresistance depending upon the manufacturing company as summarized in Table 1 of Ref. 8.

Recently RuO<sub>2</sub>-based resistors produced by Scientific Instruments Inc. (SI) are used in many laboratories, but there is no substantial publication on their magnetoresistance to the best of our knowledge. This is the motivation for our examining SI's resistors in this work. We focus on the temperature range of T < 0.3 K, where thermometry based on a physical quantity that is nominally independent of the magnetic fields is extremely troublesome, and hence, information on the magnetoresistance of resistance thermometers is extremely valuable. Note that the vapor pressure of <sup>4</sup>He or <sup>3</sup>He is no longer appropriate in this temperature range for the purpose. We have determined the magnetoresistance at temperatures down to 0.05 K in fields up to 8 T.

In addition to the magnetoresistance, we investigate the applicability of the resistors below 0.05 K. Concerning SI's resistors, the calibration is commercially available down to 0.05 K, while at present <sup>3</sup>He-<sup>4</sup>He dilution refrigerators with base temperatures of 0.02 - 0.03 K are installed in many laboratories. Hence it should be a matter of great interest how one can describe the temperature dependence of the resistance, or how well the calibration table is extrapolated to lower temperatures.

# 2 Experiment

We measured the resistance of two RuO<sub>2</sub>-based thick-film chip resistors (SI model RO-600A, S/N 1848 and 1849) at temperatures T < 0.3 K using a <sup>3</sup>He-<sup>4</sup>He dilution refrigerator. Magnetic fields up to B = 8 T were applied by means of a superconducting solenoid. The resistors are "exposed" (not canned) chips. One of them [Resister A (S/N 1848)] was placed so that the direction of the magnetic field was parallel to the film. For the other [Resistor B (S/N 1849)], the direction of the magnetic field was perpendicular to the film, and hence, perpendicular to the current flow as well. The temperature was determined by a <sup>3</sup>He-melting-curve thermometer (MCT) [12]. The MCT was placed in a region where the magnetic field was always nominally zero, i.e., magnetic fields applied for the magnetoresistance measurements were compensated in the region. Moreover, the <sup>3</sup>He melting curve is known to have a sufficiently small magnetic-field dependence in the temperature range of this work [13]. Hence, the temperature determined by the MCT is not affected by the magnetic-field applied for the magnetoresistance measurements at all.

Both the resistors and the MCT were thermally connected to the mixing chamber of the refrigerator with thick cold fingers made of pure copper or pure silver. For the resistance measurements we employed ac methods at  $f \leq$ 

25 Hz. The output voltage of the sample was detected by a voltage amplifier (DL Instruments 1201) and/or a lock-in amplifier (EG&G Princeton Applied Research 124A or Standford Research System SR830DSP) at  $T \leq 0.09$  K. At  $T \geq 0.09$  K, we used a resistance bridge (RV-Elekroniikka AVS-45). We have confirmed that the resistance obtained by the two methods agree with each other at T = 0.09 K.

#### 3 Results and discussion

#### 3.1 Magnetoresistance

The relative change of resistance  $\Delta R/R$  and of the corresponding apparent temperature  $\Delta T/T$ , i.e., temperature evaluated based on the R-T calibration table for B = 0, are shown in Figures 1 and 2, respectively, as functions of applied magnetic field for Resistors A and B. The two resistors are nominally identical (Note that their serial numbers are 1848 and 1849.) and the resistance at B = 0 agrees within 1% at all the temperatures of the magnetoresistance measurements. Hence, the orientation dependence of the magnetoresistance can be probed by comparing the results of the two resistors. One sees in Figures 1 and 2 that the orientation dependence is much smaller than the magnitude of the magnetoresistance. This characteristic is preferable from a practical point of view because the users do not have to be worried about the orientation. In usual case where the canned chip is used, one cannot even know the orientation of the film.

Now we shall look at the sign and the magnitude of the magnetoresistance. Negative magnetoresistance appears at low-field regime at T < 0.2 K, which is consistent with the information by SI [14] referring to the existence of an initial small negative magnetoresistance at temperatures below 0.25 K at low fields (less than about 1.5 T). The magnitude of the negative magnetoresistance, which is not described in Ref. 14, grows rapidly as the temperature is lowered, and at T = 0.05 K for example,  $\Delta R(B)/R(0)$  at  $B \approx 0.5$  T is -2%, which is no longer "small". In Table 1 is given  $\Delta R(B)/R(0)$  at B = 0.5 T at several temperatures. When the  $RuO_2$ -based resistors are used as thermometers, the relatively strong temperature dependence of the magnetoresistance reduce the accuracy of the temperature measurements, and hence, an appropriate care should be taken with the negative magnetoresistance. The magnetic-field dependence at higher fields, on the other hand, is simple. In Table 2, we summarize the magnetoresistance ratio of Resistors A and B determined by the experiment at high fields. The values given in the specifications [14] are also shown in the table. We find the magnetoresistance at high fields are described well by the values in the specifications.

#### 3.2 Temperature dependence in zero magnetic field

In Figure 3 the resistance is plotted as a function of  $T^{-1/4}$  in a semi-log scale. We find the temperature variation of the resistance for Resistor B at the lowest temperature range is described by

$$R(T) \propto \exp[(T_0/T)^p]. \tag{1}$$

with p = 1/4. The temperature dependence of the resistance of RuO<sub>2</sub>-based resistors at low temperatures has been analyzed in terms of variable-range hopping (VRH) conduction [3,5,7,8,10,15]. In some works [7,8,15], the exponent p was treated as a fitting parameter and various values ( $0.14 \le p < 0.71$ ) were reported. According to the theory of VRH [16], p is determined by the dimensionality d and the shape of the density of states around the Fermi level. For d = 3 and the single-particle density of states g(E) expressed by

$$g(E) \propto |E - E_F|^n,\tag{2}$$

where  $E_F$  is the Fermi energy, the exponent p is given by

$$p = \frac{n+1}{n+4}.$$
(3)

For thick-film chip resistors d = 3 is reasonable, and the very small orientation dependence of the magnetoresistance that we saw in the preceding subsection is consistent with this idea. The present result, p = 1/4, supports the constant density of states, n = 0, around the Fermi level rather than the Coulomb pseudo gap, n = 2. Good fits with p = 1/4 have also been reported for the resistors manufactured both by ALPS [3] and by Dale (RCWP575 [5], RC550 [10]).

# 3.3 Applicability below 0.05 K

At very low temperatures, resistors are easily overheated, i.e., the measured temperature can be considerably higher than the real temperature. An obvious source of the overheating is the Joule heat  $P = RI^2$  by the bias current I for the resistance measurements. Besides P, however, there can be other sources of overheating, such as the energy dissipation due to the high-frequency noise, due to the induced current by a ground loop, due to the thermoelectric power and so on. Heat conduction through the electrical leads can be other source of heat input in case of improper thermal anchoring. Because of these, it is not

an easy task to ensure the absence of overheating in experiments. Fortunately, in the present case, we can determine whether overheating is present or not, because the temperature dependence of the resistance given by Equation (1) with p = 1/4 is reasonably expected to hold even at temperatures lower than 0.05 K.

In order to estimate how small the heat flow into the resistors should be, we measured the resistance at various bias currents in zero magnetic field. In Figure 4 we show P vs. the temperature of the resistor  $T_r$  determined from its resistance. During the measurements, the temperature of the mixing chamber  $T_m$  was always lower than 6 mK. All the data points align on straight lines, i.e., a power-law relationship between P and  $T_r$  is implied. This relationship is explained in the context of the following model. First we assume that the temperature of the electron system in the resistor can be well defined even when the resistor is overheated and equals to  $T_r$ , and that the thermal impedance between the electron system and the refrigerator is proportional to  $T^{-q}$ . These assumptions lead to the relation

$$\dot{Q} = A(T_r^{q+1} - T_m^{q+1}), \tag{4}$$

at a stationary state, where  $\dot{Q}$  is the heat flow into the resistor and A is a coefficient. When overheating is extremely large, i.e.,  $T_r \gg T_m$ , the second term of the right hand side of Equation (4) can be neglected, so that

$$\dot{Q} \approx A T_r^{q+1} \tag{5}$$

holds. In addition, it is natural to expect that P is so large in this limit that it dominates  $\dot{Q}$ . Hence, it is possible to evaluate A and p in Equation (4) from a log-log plot of P vs.  $T_r$ . The dashed lines in Figure 4 represent fits of Equation (5). We obtain  $q = 2.5 \pm 0.1$  and  $\log_{10} A = -5.9 \pm 0.02$  for Resistor A, and  $q = 2.4 \pm 0.1$  and  $\log_{10} A = -6.0 \pm 0.03$  for Resistor B, where A is in units of W/K<sup>q+1</sup>. Note that  $(T_r/T_m)^{q+1} > 10^3$  for all the data points. Hence, Equation (5) is indeed an excellent approximation here.

In the opposite limit  $\Delta T \equiv T_r - T_m \ll T_m$ , i.e., when the resistor is in thermal equilibrium with the mixing chamber within a certain accuracy, an approximation

$$\dot{Q} \approx A(q+1)(\Delta T/T_r)T_r^{q+1} \tag{6}$$

holds, where  $\Delta T/T_r$  can be regarded as the accuracy of the thermal equilibrium. Since we have already determined the values of q and A, once  $\Delta T/T_r$  is given we can evaluate from Equation (6) the maximum value allowed for  $\dot{Q}$ , which is simultaneously the upper bound for P. For example, in order to

achieve  $\Delta T/T_r < 0.01$ , P < 0.2 pW is required at 30 mK and P < 5 fW at 10 mK. Keeping P sufficiently low, we measured the resistance down to 6 mK as shown in Figure 5. For T > 15 mK the resistance is described well by Equation (1) with p = 1/4, and hence the resistors are applicable. The temperature dependence of resistance levels off below 15 mK in spite of small excitation current. This leveling-off is explained if we assume the excess heat input to the resistor of about 0.1 pW.

# 4 Conclusion

We have determined the magnetoresistance of  $\text{RuO}_2$ -based resistors produced by Scientific Instruments Inc. between 0.05 K and 0.3 K in magnetic fields up to 8 T. Negative magnetoresistance is observed around 0.5 T, and its magnitude grows rapidly as the temperature is lowered. Positive magnetoresistance at high magnetic fields has smaller temperature dependence, and its magnitude is consistent with the information provided by the company. We have also investigated the characteristics of the resistors below 50 mK in zero magnetic field. The resistors are applicable down to at least 15 mK.

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Fig. 1. Relative change of resistance as a function of magnetic field for the two  $RuO_2$ -based resistors at constant temperatures. The temperatures from top to bottom in units of K are 0.05, 0.06, 0.09, 0.12, 0.16, 0.20, 0.24, respectively.

Fig. 2. Relative change of apparent temperature as a function of magnetic field at constant temperatures. The temperatures are the same as in Figure 1.

Fig. 3. Resistance as a function of  $T^{-1/4}$  for Resistor B. The line represents the best fit using the data between 0.05 K and 0.5 K. The fit is shifted downward for easier comparison.

Fig. 4. Measuring power vs. the temperature of the resistor determined from its resistance. During the measurements, the temperature of the mixing chamber was lower than 6 mK.

Fig. 5. Resistance as a function of  $T^{-1/4}$  for both the resistors.

Table 1 Magnetic-field-induced relative resistance change [R(B) - R(0)]/R(0) in units of % at B = 0.5 T.

Resistor	$0.05~{\rm K}$	0.06 K	0.09 K	0.12 K	0.16 K
А	-1.7	-1.1	-0.6	-0.2	0.0
В	-1.8	-1.0	-0.5	-0.1	0.0

Table 2

Magnetic-field-induced relative resistance change [R(B) - R(0)]/R(0) in units of % an higher magnetic fields. The results for Resistors A and B are compared with the values in Ref. 14.

	0.08 K		0.14 K				0.28 K		
	А	В	Ref. 14	А	В	Ref. 14	А	В	Ref. 14
2 T	1.0	1.3	1.4	1.5	1.8	1.3	1.3	1.4	1
4 T	3.6	4.1	4	3.7	4.0	3.4	3.1	3.3	3
6 T	6.1	6.6	7	5.6	6.0	5.3	4.5	4.7	5
8 T	8.2	8.7	8	7.3	7.7	7	5.6	5.9	6



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